

Title	Oscillation represented by the third order differential equations (part 1)
Sub Title	
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Publisher	慶應義塾大学藤原記念工学部
Publication year	1955
Jtitle	Proceedings of the Fujihara Memorial Faculty of Engineering Keio University Vol.8, No.30 (1955. ) ,p.61(1)- 67(7)
JaLC DOI	
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Notes	
Genre	Departmental Bulletin Paper
URL	<a href="https://koara.lib.keio.ac.jp/xoonips/modules/xoonips/detail.php?koara_id=KO50001004-00080030-0001">https://koara.lib.keio.ac.jp/xoonips/modules/xoonips/detail.php?koara_id=KO50001004-00080030-0001</a>

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# Oscillation Represented by the Third Order Differential Equations (Part I)

(Received August 20, 1956)

\*Hiroichi FUJITA

## Abstract

A self excited oscillation expressed by the third order differential equations is illustrated in the phase space, whose axes are displacement  $x$ , velocity  $y=dx/dt$  and acceleration  $z=d^2x/dt^2$ , respectively.

It is found that trajectories of the constant coefficient third order linear differential equation are rather simple. In aperiodic case, corresponding to the real characteristic root, the trajectories are straight lines on a cone  $y^2=xz$ ; in oscillatory case, corresponding to the complex roots, the trajectories are spiral curves on a plane  $ax+by+cz=0$ .

A nonlinear characteristic curve of a vacuum tube is divided into several sections and a linear approximation is made in each section. At the connecting point, the aperiodic component is of great importance for the balance concerning to the limit cycle, and this is one of the features of the third order oscillations.

Hartley and Colpitts oscillator are analyzed.

## I. Introduction

The oscillation involving one dependent variable is usually represented by the second order ordinary differential equation. However, if the oscillation is represented by the third order, more complicated phenomena may be represented.

## II. Phase space

In the second order ordinary differential equations, we consider the phase plane whose horizontal axis is dependent variable  $x$  and transversal axis is its derivative  $dx/dt$ . Now, in the third order differential equations, we consider a phase space. It is difficult to select the most suitable axes of phase space. But, here, the axes are dependent variable  $x$ , its derivative  $y=dx/dt$  and its second derivative  $z=d^2x/dt^2$ . When we take these axes, the trajectories are not entirely free. Let us divide the phase space into 8 quadrants. For  $z>0$ , denote  $I^+$ ,  $II^+$ ,  $III^+$  and  $IV^+$ , the four quadrants of  $x$ - $y$  plane, Denote  $I^-$ ,  $II^-$ ,  $III^-$  and  $IV^-$  the four corresponding quadrants of  $z<0$ . Then, in  $I^+$ , since  $y=\dot{x}>0$ ,  $x$  increases and since  $z=\dot{y}>0$ ,  $y$  increases too. As the result, in  $I^+$  and  $III^-$ , the trajectories go away from the origin. In the contrary, in  $IV^-$  and  $II^+$ , they come to the origin. In  $III^+$ ,  $II^+$ ,  $I^-$ , and  $IV^-$

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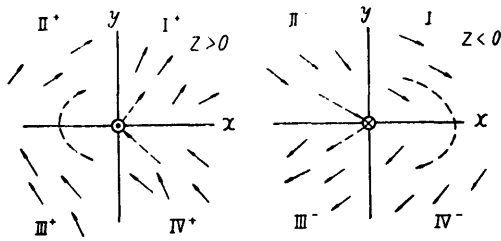


Fig. 1

the trajectories turn around the origin in this order. As described later, the trajectories corresponding to periodic solutions turn on these quadrants in this order. The extremity of  $x$  is on the  $xz$  plane and the extremity of  $y$  is on the  $xy$  plane.

**III. Singular points**

Let  $x$  be variation of voltage or current. The differential equation for the oscillator of the third order are generally

$$\frac{dx}{dt} = y \quad \frac{dy}{dt} = z \quad \frac{dz}{dt} = f(x, y, z) \quad f(0, 0, 0) = 0$$

At the origin, the directions of trajectories can not be decided, so the origin is a singular point. In the neighbourhood of origin, the trajectories of general nonlinear differential equation coincide with the trajectories of the third order constant coefficient linear differential equation.

The differential equation has three characteristic roots. If the roots are complex, they are conjugate. Thus their characteristic roots will accord with one or other of the following 8 cases:

- |                 |                       |                    |              |              |
|-----------------|-----------------------|--------------------|--------------|--------------|
| (i) $-\lambda$  | $-\alpha \pm j\omega$ | (v) $-\lambda_1$   | $-\lambda_2$ | $-\lambda_3$ |
| (ii) $-\lambda$ | $\alpha \pm j\omega$  | (vi) $\lambda_1$   | $-\lambda_2$ | $-\lambda_3$ |
| (iii) $\lambda$ | $-\alpha \pm j\omega$ | (vii) $\lambda_1$  | $\lambda_2$  | $-\lambda_3$ |
| (iv) $\lambda$  | $\alpha \pm j\omega$  | (viii) $\lambda_1$ | $\lambda_2$  | $\lambda_3$  |

where all letters are real positive numbers. (i) and (v) are stable and the others are all unstable.

**IV. The trajectories of the third order constant coefficient linear differential equations.**

In order to know the rough characteristics of trajectories of nonlinear differential equations, it is necessary to investigate the third order constant coefficient linear differential equations.

**IV-1 Case of non-periodic solutions**

When a characteristic root is real, say  $\lambda_1$ ,

$$(4-1) \quad \begin{cases} x = Ke^{\lambda_1 t} \\ y = \lambda_1 Ke^{\lambda_1 t} = \lambda_1 x \\ z = \lambda_1^2 x = \lambda_1 y \end{cases}$$

Where  $K$  is an arbitrary constant. (4-1) are equations of lines passing through the origin, that is

$$(4-2) \quad \begin{cases} y = \lambda_1 x \\ z = \lambda_1 y \end{cases}$$

For any  $\lambda_1$ , the line is on the corn

$$(4-3) \quad y^2 = xz$$

The axis of this corn is

$$(4-4) \quad \begin{cases} x = z \\ y = 0 \end{cases}$$

and angle of vertex is  $\pi$ . Near the  $z$  axis on the corn, representative point moves rapidly. In  $I^+$  it moves to infinity and in  $IV^+$ , to origin.

When a differential equation has three real characteristic roots, the general solution is represented by linear combination of three non-periodic solutions.

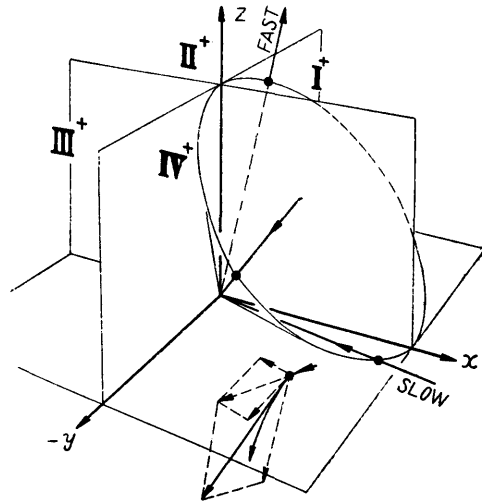


Fig. 2

Define a vector whose direction is tangential to the trajectory and whose amplitude is the velocity of representative point. Then the vector of nonperiodic general solution is decomposed to three vectors which are parallel with the trajectories on the corn corresponding to  $K_i e^{\lambda_i t}$  ( $i=1, 2, 3$ .)

(Let us called these trajectories nonperiodic solution axes.)

The decomposition and composition of these vectors are done by the parallel quadrilateral method. No trajectories cross a plane decided by the two nonperiodic solution axes and trajectories on this plane never go out from this plane.

#### IV-2 Plane of periodic solution

When the characteristic roots are complex conjugate, the solution is periodic.

Then

$$(4-5) \quad \begin{cases} x = Ae^{-\alpha t} \sin(\omega t + \varphi) \\ y = Ae^{-\alpha t} \{ \omega \cos(\omega t + \varphi) - \alpha \sin(\omega t + \varphi) \} \\ z = Ae^{-\alpha t} \{ (\alpha^2 - \omega^2) \sin(\omega t + \varphi) - 2\alpha\omega \cos(\omega t + \varphi) \} \end{cases}$$

Where  $A$  and  $\varphi$  are arbitrary constants, From (4-5), eliminate  $\sin(\omega t + \varphi)$   $\cos(\omega t + \varphi)$  and  $e^{-\alpha t}$ , and obtain the followid

$$(4-6) \quad (\alpha^2 + \omega^2)x + 2\alpha y + z = 0$$

(4-6) is the equation of plane.

This plane intersects  $yz$  plane ( $x=0$ ) along the  $z=-2\alpha y$  and  $xz$  and  $xy$  planes along the lines  $z=-(\alpha^2 + \omega^2)x$  and  $y=-(\alpha^2 + \omega^2)x/2\alpha$ . In fig. 3,  $D$  is a plane for damped oscillating solution and  $I$  is a plane for increased one.

For high frequency oscillation, the velocity and acceleration are large, and an angle between the periodic solution plane and  $yz$  plane is small. General solution which contains periodic component, has a vector turning clockwise on the plane.

So, trajectories are on an exponential horn or a hyperbolic horn.

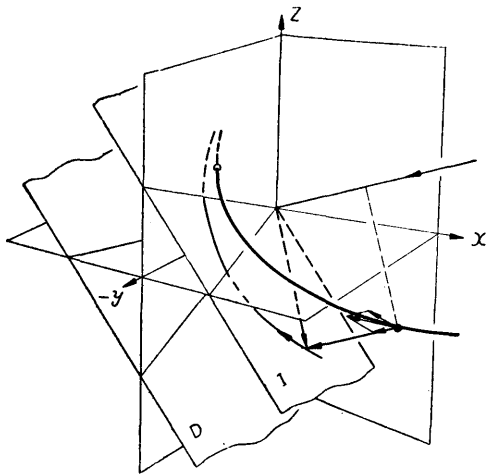


Fig. 3

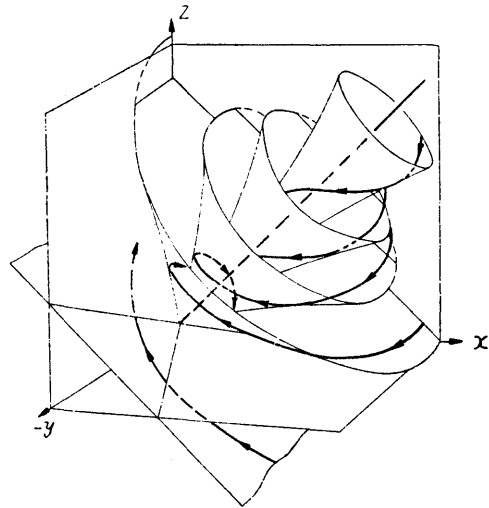


Fig. 4

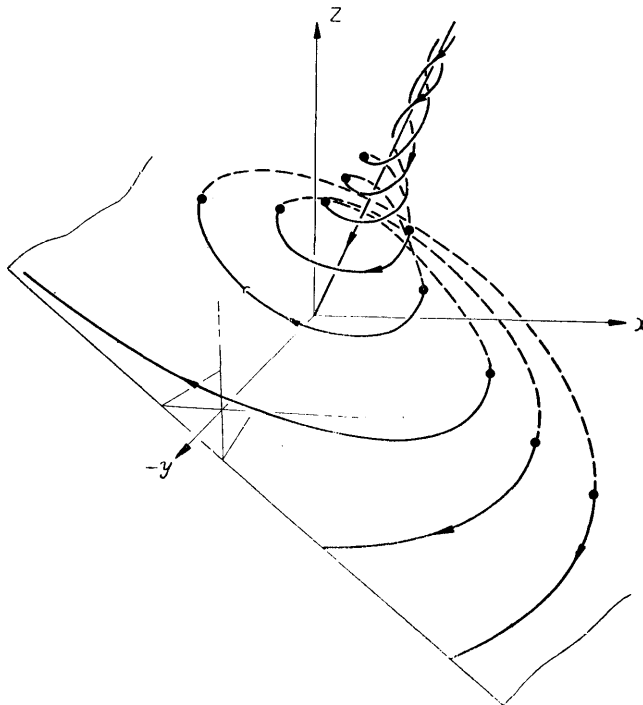


Fig. 5

### V. Oscillators represented by the third order nonlinear differential equations.

We will apply the above representation to the analysis of oscillators. At first,

Hartley and Colpittz oscillator are analyzed.

**V-1 Hartley oscillator**

Using notation shown in fig. 6, we obtain the circuit equation for grid voltage

$$V_g \equiv x$$

$$L_p L_g C \frac{d^3 f(x)}{dt^3} + (L_p R_g + L_g R_p) C \frac{d^2 f(x)}{dt^2} + (L_p + L_g) C \frac{d^2 x}{dt^2}$$

$$+ (R_p + R_g) C \frac{dx}{dt} + R_p R_g C \frac{df(x)}{dt} + x = 0 *$$

where  $-f(x) = i_p$  neglecting grid current.

Grid current plays an important role in the oscillator but in order to simplify the problem, we neglect it here and later (part II) we will consider it in grid tuned oscillator.

For the convinience of numerical

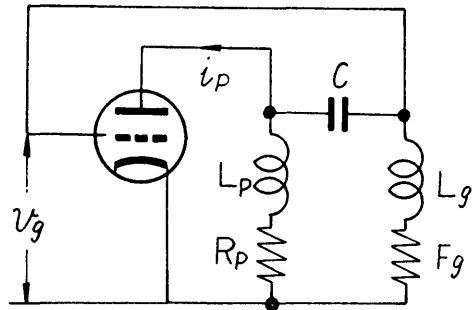


Fig. 6

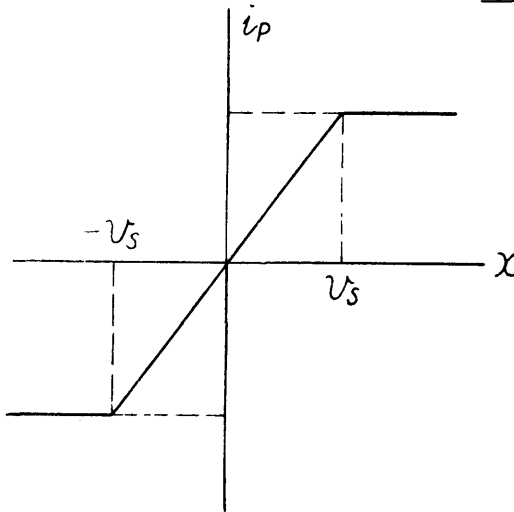


Fig. 7

calculation, let the time normalize

$$\omega t = \tau$$

where  $\omega$  is an angular frequency of oscillator decided by linear network theory.

The nonlinear characterisitic of vacuum tube is divided into three sections and approximated by linear characteristics in each sections, shown in fig. 7 Denote  $V_s$  as critical value between linear zone and satulating zone.

For  $|x| < V_s$  (linear zone)

$$g_1 \ddot{x} + (1+g_2) \dot{x} + \sqrt{\frac{c}{L_p+L_g}} (g_3+R_p+R_g) \dot{x} + x = 0$$

$|x| > V_s$  (satulating zone)

$$\ddot{x} + \sqrt{\frac{c}{L_p+L_g}} (R_p+R_g) \dot{x} + x = 0$$

\*H. Fujita, This Proceedings, 7. 29 (1954)

where

$$g_1 \equiv \omega^3 L_p L_g C g_m$$

$$g_2 \equiv \omega^3 C (L_p R_g + L_g R_p) g_m$$

$$g_3 \equiv R_p R_g g_m$$

For ordinary circuit elements of oscillator, the origin in the phase space is singular point (ii). In the satulating zone, the differential equation has the complex

characteristic roots whose real parts are negative and the trajectories lie only on the plane of periodic solution.

If a small initial deviation from the origin is given, the representative point reaches at  $|x| = V_s$  on the plane of increasing periodic solution of linear zone, for nonperiodic component will become negligibly small.

At  $|x| = V_s$  representative point jumps onto the plane of decreasing periodic solution of satulating zone. Here, the solution and its derivative are continuous and second derivative is discontinuous. If the characteristics of vacuum

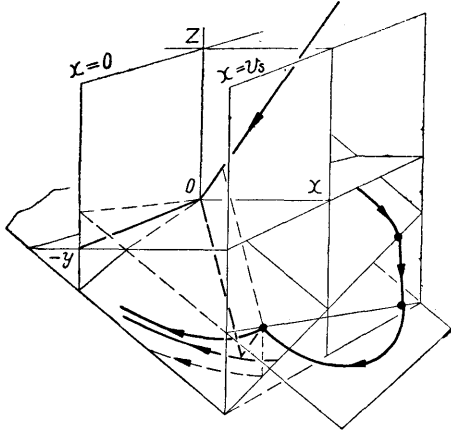


Fig. 8

tube has continuous derivative, the representative point does not jump but comes very rapidly to the plane of satulating zone.

From here, the representative point goes through the maximum value of  $x$  and comes to  $|x| = V_s$  again and enters the linear zone. But here the representative point is not on the plane of periodic solution.

So, the solution must have nonperiodic component. Therefore the periodic component is suppressed. This suppression at the boundary plane between linear and satulating zones does not occur in oscillations represented by the second order differential equations.

*On the limit cycle.*

The increase in the linear zone and the decrease in the satulating zone and at boundary planes  $x = V_s$ , are balanced. Then the solution is stately periodic.

## V-2. Colpittz oscillator

The differential equations for the Colpittz oscillator are obtained in the same way as for the Hartley oscillator.

In the linear zone

$$\ddot{x} + R\dot{x} + \dot{x} + gx = 0$$

and in the satulating zone

$$\ddot{x} + R\dot{x} + \dot{x} + i_{p0} = 0$$

where  $R \equiv r/\omega L = \frac{1}{Q}$   
 $g = g_m/\omega(C + C_g)$

In the linear zone, trajectories are same type as the Hartley oscillator. But in the saturating zone, the solution is

$$x = Ae^{-Rt/2} \sin(\omega t + \varphi) - i_{po}t + K$$

where  $A$ ,  $\varphi$  and  $K$  are arbitrary constants.

Therefore, in saturating zone, the nonperiodic axis is on  $x$ - $y$  plane and parallel to  $x$  axis. So representative point is on exponential horns shown in fig. 10.

Physical meaning of  $-i_{po}t$  is constant current discharge from  $C_g$  in saturating zone. Stately periodic trajectory occurs in the same way as with the Hartley oscillator.

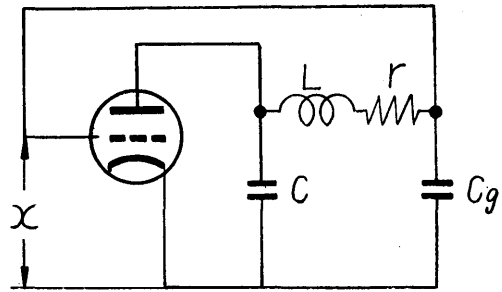


Fig. 9

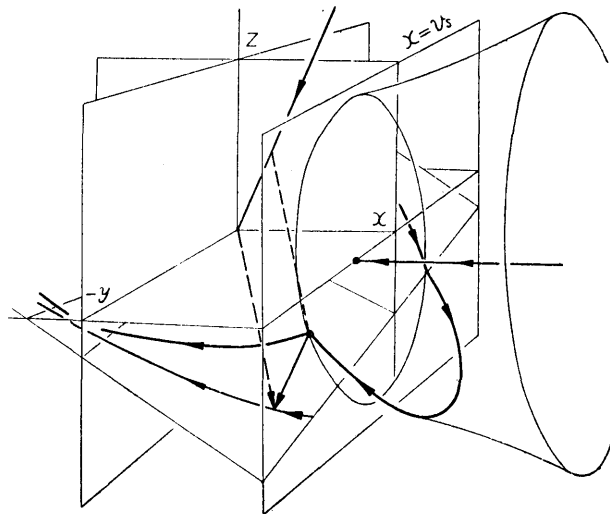


Fig. 10